$$(z^{p} + u_{1}z^{p-1} + \dots + u_{p}) + 5 \quad (\beta_{0} z^{p} + \beta_{1}z^{p-1} \dots + \beta_{p}) = 0$$

$$F_{N}(z)$$

$$F_{T}(z)$$

BE method: « = 1, « = -1, β = -1 (1st order Gear's method or BDF)

Variable time steps
h is no longer uniform

$$\sum_{i=0}^{p} \alpha_i \alpha_{n-i} + h \beta_i \alpha_{n-i} = 0$$
 LMS method

with
$$\sum_{n=0}^{1} \beta_{i} = -1$$
 for LE calculations
Example 2nd order Gear's method (BDF)
 $\sum_{n=0}^{2} \alpha_{i} \chi_{n-i} - h_{n}\chi_{n} = 0$
 $\chi_{0} \chi_{n} + \alpha_{1}\chi_{n-1} + \alpha_{2}\chi_{n-2} - h_{n}\chi_{n} = 0$
For a 2nd order method $\Rightarrow exact for$
polynomials of degree ≤ 2
Take $P(t) = (t-t_{n})^{\times}$ $K=0, 1, 2$
 $K=0$: $\chi(t) = 1$ $\dot{\chi}(t) = 0$
 $K=1$: $\chi(t) = (t-t_{n}) - \dot{\chi}(t) = 1$
 $K=2$: $\chi(t) = (t-t_{n})^{2} \chi(t) = 2(t-t_{n})$
For LE calculation we use exact solution
 $K=0$: $\chi_{0}\chi(t_{n}) + \alpha_{1}\chi(t_{n-1}) + \alpha_{2}\chi(t_{n-2}) - h_{n}\chi(t_{n}) = 0$
 $d_{0} + \alpha_{1} + \alpha_{2} = 0$

K=1:
$$d_{0}(0) + d_{1}(t_{n-1}-t_{n}) + d_{2}(t_{n-2}-t_{n}) - h_{n} = 0$$

(-h_{n}) - (h_{n} + h_{n-1})

K= 2;

$$d_{0} = h_{n} \left(\frac{1}{h_{n}} + \frac{1}{h_{n} + h_{n-1}} \right)$$

All coefficients are dependent on the timestep In General for K-th BDF ($1 \le \text{order} \le k$) $d_0 = hn \sum_{i=1}^{k} \frac{1}{t_n - t_n - i}$

$$1 \le j \le k: \quad dj = \frac{h_0}{(t_n + t_n)} \prod_{\substack{k=1 \ k=1}}^{k} \frac{t_n + t_n \cdot i}{(t_n - t_n \cdot i)}$$

$$F_X: \quad 2nd \quad order \quad & \text{BDF}$$

$$d_0 = h_n \sum_{\substack{k=1 \ k=1}}^{2} \frac{1}{t_n + t_{n-1}} = h_n \left[\frac{1}{t_n - t_{n-1}} + \frac{1}{t_n + t_{n-1}} \right]$$

$$a_1 = \frac{h_n}{(t_n - t_{n-1})} \prod_{\substack{k=1 \ k=1}}^{2} \frac{t_n - t_n \cdot i}{t_{n-1} - t_{n-1}}$$

$$= -\frac{h_n}{h_n} \quad \frac{t_n - t_{n-2}}{t_{n-1} - t_{n-2}} = -\frac{h_n + h_{n-1}}{h_{n-1}}$$
For KHA order BDF LE

$$C_{k+1} = \frac{1}{(k+1)!} \frac{1}{h_n} \prod_{\substack{k=1 \ k=1}}^{k} \left(t_n - t_{n-1} \right)$$
Where $LE = C_{k+1} h_n^{k+1} (k + y)(t_n)$

$$ket \quad us \quad consider TR$$

$$Uniform h: \quad x_n = x_{n-1} + \frac{h}{2} (x_n + x_{n-1})$$
Non uniform $d_0 x_n + d_1 x_{n-1} + h_n \beta_0 x_n + h_n \beta_1 x_{n-1} = 0$
Some ω TR with uniform h

$$LE = -\frac{h_{n}^{3}}{12} \tilde{x}(t_{n})$$
Timestep control
How do we determine the stepsize hn?
Goal: choose as fewer timepoints as possible
guen an error constraint
 \Rightarrow =minimize # of timepoints
Assume En is abound on the absolute
error $[LE_{n}] \leq E_{n}$
 $[LE_{n}] = [C_{k+1} h_{n}^{k+1} \chi^{(k+1)}(t_{n})] \leq E_{n}$
 $h_{n} \leq [\frac{E_{n}}{[C_{k+1} \chi^{(k+1)}(t_{n})]}]^{k+1}$

En is quen,
$$C_{u+1}$$
 is known
What about $z^{(k+1)}(t_n)$?
In SPICE divided differences are used
 $DD_1 = \frac{x_n - x_{n-1}}{h_n} \cong x_n$
 $DD_2 = \frac{DD_1(t_n) - DD_1(t_{n-1})}{h_n + h_{n-1}} \cong \frac{x_n}{2!}$
 $DD_{k+1} = \frac{DD_k(t_n) - DD_k(t_{n-1})}{\sum_{1=0}^{k} h_{n-i}} \frac{(k_{n+1})}{(K+1)!}$
 $\frac{Order Control}{If}$
If we have a method of order K
(BDF: $1 \le K \le 6$)

-> Choose order which gives you the largest timestep 1 LE K=3 K=2 1 K=1 E3 E١ > h. In SPICE the default method is TR (METHOD = GEAR MAXORD = N (2 ≤ N ≤ 6) Heurishic rules for timestep control · Do not change timestep too often · Change order only it improvement is worthwhile i.e. at least 2h · Attempt change of stepsize and order only if [LE] < En (error is large) In SPICE: En = GA + GR MAX (|×nl, |×n-1) ABSTOL (Currents) VNTOL (Voltages CHGTOL (Charges

Linear Multistep Methods – Stability

$$\sum_{i=0}^{p} \alpha_{i} \mathbf{x}_{n-i} + h \beta_{i} \dot{\mathbf{x}}_{n-i} = \mathbf{0}; \text{Testproblem} \frac{d}{dt} \mathbf{x}(t) = \lambda \mathbf{x}(t), \mathbf{x}(0) = 1 \tag{1}$$

$$\sum_{i=0}^{p} \left(\alpha_{i} + \beta_{i} h \lambda \right) \mathbf{x}_{n-i} = \sum_{i=0}^{p} \left(\alpha_{i} + \sigma \beta_{i} \right) \mathbf{x}_{n-i} = \mathbf{0}$$
(2)

- A method is stable if all solutions of the associated difference equation (2) obtained by setting σ=0 remain bounded as n→∞
- The region of absolute stability of a method is the set of σ (complex) such that all solutions of (2) remain bounded as n→∞
- Note: A method is stable if its region of absolute stability contains the origin, i.e., σ=0

Stability

The region of absolute stability of a method is the set of σ such that all the roots of $\sum_{i=0}^{p} (\alpha_i + \sigma \beta_i) z^{p-i} = 0$ are inside or on the complex unit circle, i.e., $|z| \leq 1$, and the roots for which |z| = 1 are of multiplicity 1

A method is A-stable if the region of absolute stability contains the entire left-half plane ($Re(\sigma)<0$) TR is an A-stable method



Stability

- Each method is associated with two polynomials of coefficients α and β:
 - α: associated with past function values (x_{n-i})
 - β: associated with past derivative values (x'_{n-i})
- Stability: roots of α polynomial must satisfy |z|≤1 and be of multiplicity 1 for |z|=1
- Absolute stability: roots of (α+ σβ) polynomial must satisfy |z|≤1 and be of multiplicity 1 for |z|=1

Stability and Region of Absolute Stability



From: A. Nardi





L-Stability

• An A-stable method is L-stable if $Re(\lambda) < 0$ implies $\lim_{h \to \infty} x_n = 0$ for all x_{n-1}

Consider TR Re(
$$\lambda$$
) < 0 : $\mathbf{x}_n - \mathbf{x}_{n-1} - \frac{\mathbf{h}}{2} (\dot{\mathbf{x}}_n + \dot{\mathbf{x}}_{n-1}) = 0$
 $\left(1 - \frac{\lambda \mathbf{h}}{2}\right) \mathbf{x}_n - \left(1 + \frac{\lambda \mathbf{h}}{2}\right) \mathbf{x}_{n-1} = 0$
 $\Rightarrow \mathbf{x}_n = \frac{\left(1 + \frac{\lambda \mathbf{h}}{2}\right)}{\left(1 - \frac{\lambda \mathbf{h}}{2}\right)} \mathbf{x}_{n-1} \Rightarrow \lim_{\mathbf{h} \to \infty} \mathbf{x}_n = -\mathbf{x}_{n-1}$

i.e., there is ringing

TR in not an L-stable method

Finding the Region of Absolute Stability

 $(1+\sigma\beta_0)z^p+(\alpha_1+\sigma\beta_1)z^{p-1}+\ldots(\alpha_p+\sigma\beta_p)=0$

For what values of σ do all the p roots of this polynomial satisfy the stability condition?

$$z^{p} + \alpha_{1} z^{p-1} + \dots + \alpha_{p} + \sigma \left(\beta_{0} z^{p} + \beta_{1} z^{p-1} + \dots + \beta_{p}\right) = 0$$

Methods

- 1. Choose σ , compute roots, test, repeat for all σ (BAD)
- 2. Solve for σ =-P_N(z)/P_D(z) P_N(z) = z^p + $\alpha_1 z^{p-1}$ + ... α_p P_D(z) = $\beta_0 z^p$ + $\beta_1 z^{p-1}$ + ... β_p

Consider S =
$$\left\{ \sigma \middle| \sigma = -\frac{P_{N}(z)}{P_{D}(z)}, |z| \le 1 \right\}$$
 and let z vary in $|z| \le 1$

May get same σ values for two or more different z's, one with $|z| \le 1$ and one with |z| > 1 \Rightarrow S is a superset of the region of absolute stability

Boundary Locus Γ_{σ}

Boundary locus Γ_{σ} is the contour $-\frac{P_{N}(z)}{P_{n}(z)}$ when |z| = 1, i.e., $z = e^{j\theta}$,

 $0 \leq \theta \leq 2\pi.$ It is a map from the z -plane to the σ -plane



Basic Results from Theory of Complex Variables

- Mapping is conformal, i.e., angle preserving
- Γ_{σ} separates the σ -plane into disjoint sets. In each set, the number of roots outside the unit circle is constant
- The boundary of the stability region is a subset of Γ_σ

Region of Absolute Stability

Move counterclockwise along |z|=1, then you see one more root to the outside of the unit circle for those σ to the right than for those σ to the left when traversing Γ_{σ}



Large Timestep Issues Stiff Problems

$$\begin{cases} \frac{d\mathbf{x}(t)}{dt} = -\lambda_1(\mathbf{x} - \mathbf{s}(t)) + \frac{d\mathbf{s}(t)}{dt} & \text{where} \quad \mathbf{s}(t) = \mathbf{1} - e^{-\lambda_2 t} \\ \mathbf{x}(0) = \mathbf{x}_0 & \lambda_1 = \mathbf{10}^6, \lambda_2 = \mathbf{1} \\ \text{Exact solution :} \quad \mathbf{x}(t) = \mathbf{x}_0 e^{-\lambda_1 t} + \mathbf{1} - e^{-\lambda_2 t} \\ \mathbf{x}_0 e^{-\lambda_1} & \text{For } t \ge 5 \cdot \mathbf{10}^{-6} & \mathbf{x}_0 e^{-\lambda_1 t} \approx \mathbf{0} \\ \mathbf{x}_0 e^{-\lambda_1} & \text{For } t \ge 5 \cdot \mathbf{10}^{-6} & \mathbf{x}_0 e^{-\lambda_1 t} \approx \mathbf{0} \\ \text{For } t \ge 5 & \mathbf{1} - e^{-\lambda_2 t} \approx \mathbf{1} \\ \text{Interval of interest is [0,5]} \\ \text{Uniform step size (for accuracy)} \\ \Rightarrow \Delta t \le \mathbf{10}^{-6} \\ \Rightarrow 5\mathbf{x}\mathbf{10}^{-6} & \text{steps !!!} \\ \end{cases}$$

One Possible Strategy – Variable Time Steps

- Take 5 steps of size 10⁻⁶ for accuracy during initial phase and then 5 steps of size 1
- With FE cannot use h > 2×10^{-6} (λ = 10^{6})

Stiff problem:

- 1. Natural time constants
- 2. Input time constants
- 3. Interval of interest

If these are widely separated, then the problem is stiff



With BE can use small timesteps for fast dynamics and then switch to large timesteps for the slow decay

From: A. Nardi

· A-stable methods satisfy this requirement

From: A. Nardi

Requirements of Stiffly Stable Integration Methods

For accuracy want at least 8 points per cycle

 $\Rightarrow h \leq \frac{1}{8} \left(\frac{2\pi}{b_i} \right) \text{ or } hb_i \leq \frac{\pi}{4} \Rightarrow Im(\sigma) \leq \frac{\pi}{4}$

Requirements of Stiffly Stable Integration Methods

Want a region of absolute stability which gives a stable algorithm for initial transient



 $\Rightarrow a_i h > 0, a_i h < \mu$ $Re(\sigma) = a_i h$ $Require : 0 \le Re(\sigma) \le \mu$

Requirements of Stiffly Stable Integration Methods

Require a small h to capture fast transient



Remarks:

- There is a region $Re(\sigma) < -\delta$ that is absolutely stable
- For 0 < Im(σ)< π/4 the region is of absolute stability and the algorithm is accurate
- For 0 < Re(σ)<μ the region is stable and the algorithm is accurate

Backward Differentiation Formula -BDF (Gear Methods)

$$\sum_{i=0}^{k} \alpha_{i} \boldsymbol{x}_{n-i} + h \beta_{0} \dot{\boldsymbol{x}}_{n} = 0 \qquad \text{whe re} \quad \beta_{0} \neq 0$$

- Gear's first order method is BE
- It can be shown that:
 - Gear's methods up to order 6 are stiffly stable and are well-suited for stiff ODEs
 - Gear's methods of order higher than 6 are not stiffly stable
- Less stringent than A-stable



Gear's Method Region of Absolute Stability Gear's Met (outside the closed curve) Gear's Met

Gear's Method Region of Absolute Stability (outside the closed curve)



Observations on Stiff Stability

- FE: timestep is limited by stability and not by accuracy
- BE: A-stable, any timestep could be used
- TR: most accurate A-stable multistep method
- Gear: stiffly stable method (up to order 6)
- The analysis of stiff circuits requires the use of variable timestep