

HW # 4 part 2 Due by Thu 5pm
 Project proposals Due Monday in class

Exam Monday Nov. 21 2-3:50pm
 more on it later

HW # 3 - Part 1 graded handed back

BJT Colpitts oscillator

Asymptotic Waveform Evaluation (AWE)

$$F(s) = \underbrace{m_0}_{\leftarrow} + \underbrace{m_1 s}_{\leftarrow} + \underbrace{m_2 s^2}_{\leftarrow} + \dots - m_n s^n + \dots$$

moments

General Method

$$(G + sC) x = b$$

$$y = l^T x$$

$$\underline{x} = \underline{m}_0 + \underline{m}_1 s + \underline{m}_2 s^2 + \dots$$

Impulse response $b = 1$

$$(G + sC) (m_0 + m_1 s + m_2 s^2 + \dots) = b$$

$$G m_0 = b$$

$$(G m_1 + C m_0) = 0$$

$$\vdots$$

$$(G m_i + C m_{i-1}) = 0$$

Solve for m_0 by LU Factoring G and doing forward/back solves

$Gm_i = -Cm_{i-1}$
 m_i can be determined by forward/back solves

$$m_0 = G^{-1}b$$

$$m_1 = -G^{-1}CG^{-1}b$$

⋮

$$m_i = (G^{-1})^{i+1}C^i b$$

$(G^{-1})^i$ can be very ill conditioned

AWE is limited to about 10 poles because of numerical ill conditioning

A robust method is PVL (Padé via Lanczos)

(paper posted on website)

Problem with Padé approximation (unstable reduced systems)

$$H(s) = \frac{K_1}{s-p_1} + \frac{K_2}{s-p_2} ; H_{0,1} = \frac{K}{s-p}$$

$$= \frac{-K_1}{p_1} \frac{1}{1-\frac{s}{p_1}} + \frac{-K_2}{p_2} \frac{1}{1-\frac{s}{p_2}}$$

$$= \frac{-K_1}{p_1} \left[1 + \frac{s}{p_1} + \frac{s^2}{p_1^2} + \dots \right] - \frac{K_2}{p_2} \left[1 + \frac{s}{p_2} + \frac{s^2}{p_2^2} + \dots \right]$$

$$H_{0,1}(s) = \frac{K}{s-p} = \frac{-K}{p} \left[1 + \frac{s}{p} + \frac{s^2}{p^2} + \dots \right]$$

$$\left. \begin{aligned} \frac{K}{p} &= \frac{K_1}{p_1} + \frac{K_2}{p_2} \\ \frac{K}{p^2} &= \frac{K_1}{p_1^2} + \frac{K_2}{p_2^2} \end{aligned} \right\} \Rightarrow p = \frac{\frac{K_1}{p_1} + \frac{K_2}{p_2}}{\frac{K_1}{p_1^2} + \frac{K_2}{p_2^2}}$$

Suppose $K_1 = 3, K_2 = -8, p_1 = -1, p_2 = -2$

$$p = \left[\frac{3}{-1} + \frac{-8}{-2} \right] / \left(\frac{3}{1} + \frac{-8}{4} \right) = 1$$

Exam

closed book / "closed" notes

2-page of notes 8½" x 11" paper

Use the sample exam as a guide

Topics:

→ Nodal or MNA Stamps

→ Solution of nonlinear eqns
(Newton method)

nonlinear component → Companion
network
model

$$f(x) = 0$$

$$J_x^{k+1} = J_x^k - f(x^k)$$

until convergence

Stamping of nonlinear elements

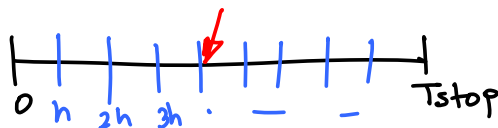
→ Transient analysis

- given an integration method of order k , step p

- Exactness constraints
- Local Error
- Stability of the method & regions of absolute stability

Application to circuits:

- Companion network at timepoint t_n
linear / nonlinear component



$$\dot{x}_n = \underline{\alpha} x_n + \underline{\beta}$$

implicit method

inductors, capacitors → Linear

nonlinear capacitors (charge-based formulation)

Simulation of Radio Frequency Integrated Circuits

Based on:

“Computer-Aided Circuit Analysis Tools for RFIC Simulation: Algorithms, Features, and Limitations,” *IEEE Trans. CAS-II*, April 2000.

Outline

- Introduction
- Analyses required for RF circuits
- SPICE analyses and limitations
- Algorithms for RF simulation
 - Time-domain methods
 - Harmonic-balance method
 - Mixed time-frequency methods
 - Envelope method
 - Linear time varying analysis
- RF noise
- Commercial tools

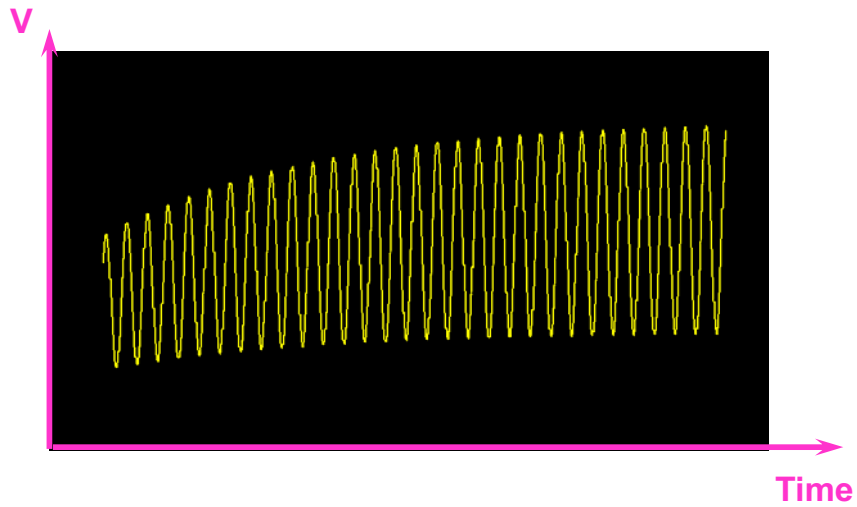
Introduction

- RF blocks are a big challenge in the design process
- Typical blocks that are analyzed
 - Amplifiers
 - Mixers
 - Oscillators, Voltage Controlled Oscillators (VCOs)
 - Phase-Locked Loops (PLLs)
 - Filters (CT, SC, SAW)
- SPICE is not adequate for circuit level analysis of most RF blocks
- Lack of computer-aided analysis tools aggravates design problems

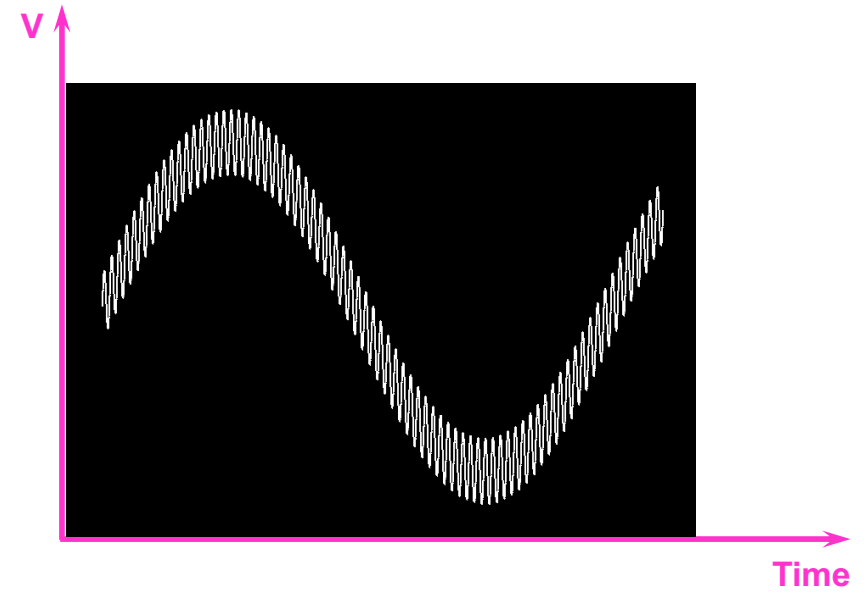
Analyses Required for RF Circuits

- Rapid simulation of the periodic or quasi-periodic steady state
- Accurate simulation of harmonic and intermodulation distortion
- Simulation of noise up/down conversion due to circuit nonlinearities
- Phase noise/jitter simulation
- Simulation of oscillator turn-on transient
- Simulation of the capture process of PLLs
- Distributed element simulation

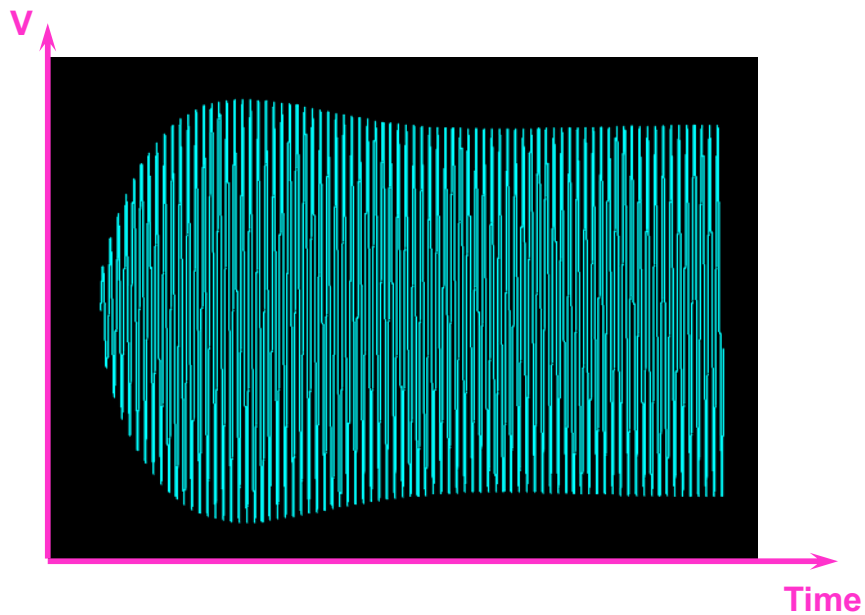
RF Amplifier Periodic Steady State



Mixer Quasi-Periodic Steady State



Oscillator Turn-On and Steady State



SPICE Analyses and Applications

- **DC**
 - .op, .dc
 - Dc operating point, dc transfer curves
 - Can be used for all circuits
- **Small-signal AC**
 - .ac, .noise, .disto
 - Frequency response of linearized circuits
 - Can be used for amplifiers

SPICE Analyses and Applications

- **Transient**
 - .tran, .four
 - Large-signal time-domain analysis
 - Can be used for
 - Amplifiers
 - Oscillators
 - Mixers
 - PLLs
 - A/D, D/A converters

SPICE Limitations

- **Noise analysis at a dc operating point**
 - Cannot simulate noise mixing in mixers
 - Cannot simulate phase noise/jitter
- **Long transient analyses required for**
 - Periodic/quasi-periodic steady state
 - Turn-on transients of high-Q oscillators and capture process of PLLs
 - **Can accumulate significant numerical error**

SPICE Limitations

- **Fourier analysis**
 - Requires periodic steady state and fundamental frequency
 - Multiple tones must be commensurate
 - IM3 simulation is difficult
 - Subject to interpolation and aliasing errors
 - Tighter tolerances required to resolve small harmonics
 - **Fourier integral gives reliable results**
- **Elements and models**
 - Transmission line is the only distributed element
 - Models may possess discontinuities in higher-order derivatives => **spectral contamination**

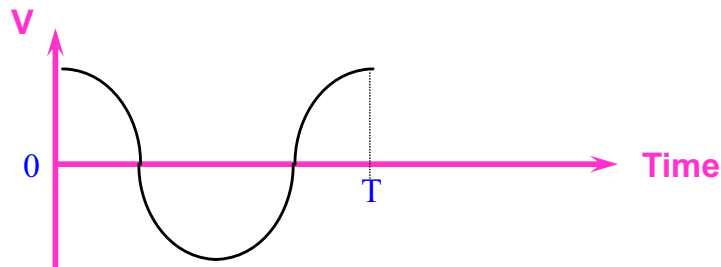
Periodic Steady-State Simulation

- **Time-domain methods**
- **Harmonic-balance method**
- **Mixed time-frequency methods**
- **Traditionally limited to small circuits**
- **Recent advances allow simulation of much larger circuits**

Time-Domain Method

- Impose periodicity constraint

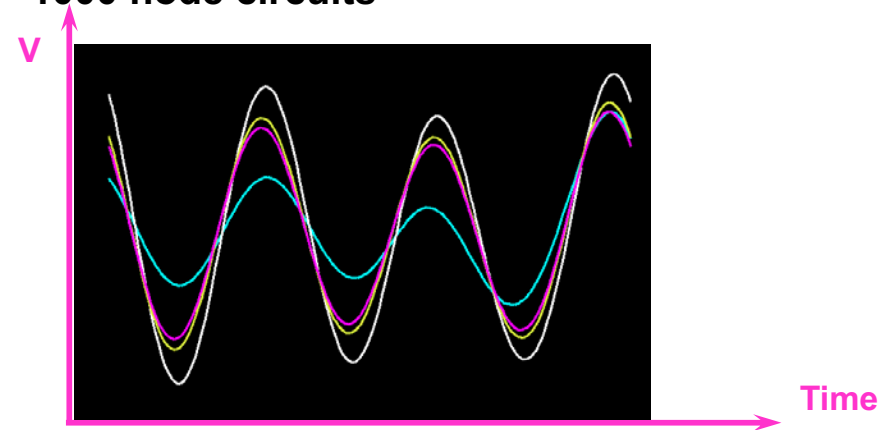
$$v(0) = v(T)$$



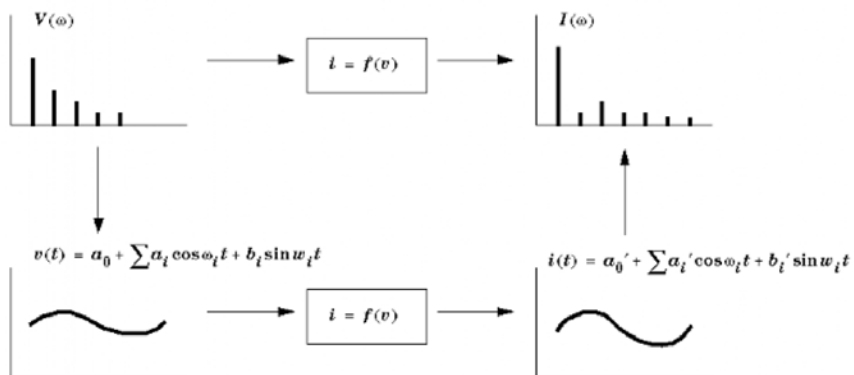
- For a driven circuit period T is known
- For an oscillator T is an unknown

Time-Domain Method

- A popular method is the shooting method
- Requires dense matrix solutions
- Matrix-free methods allow simulation of ~1000 node circuits

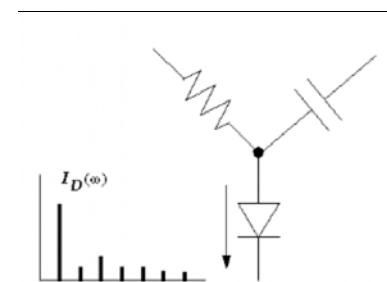


Non-Linear Frequency Domain Analysis



- Low distortion signals require few Fourier series coefficients
- Smooth device models are essential for RF

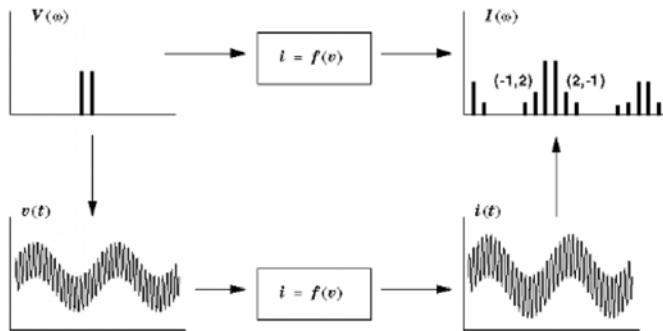
Harmonic Balance



- “Balance” the frequency spectrum at each node

- Time-derivatives (capacitors) become multiplication in frequency domain
- Handle distributed elements in freq. domain

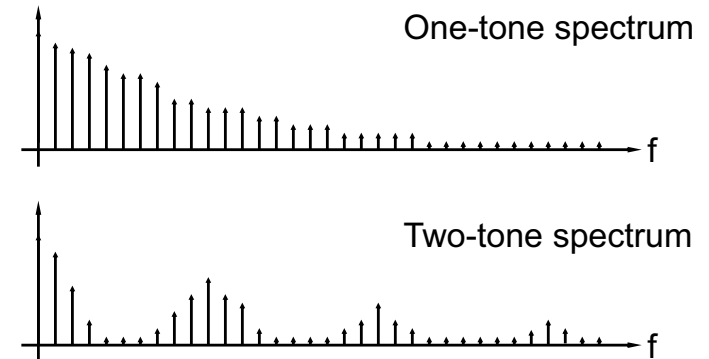
Multi-Tone Frequency Domain Analysis



- **Minimum number of “time-domain” samples dictated by the number of significant Fourier coefficients, not by the Nyquist rate**

Frequency Truncation

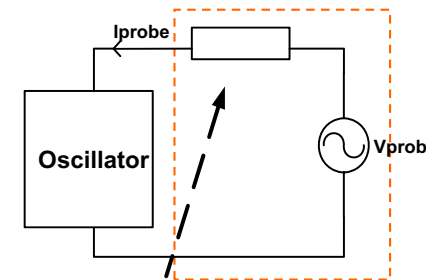
- Harmonic truncation
 - keep a finite number of frequencies containing significant energy



Oscillator Simulation with HB

- **Problems**
 - Unknown period of oscillation
 - Arbitrary time origin
- **Solutions** (K. Kundert, 1990)
 - Frequency as an additional unknown
 - Additional equation to fix phase
- Direct implementation \Rightarrow convergence problems

Use Voltage Probe



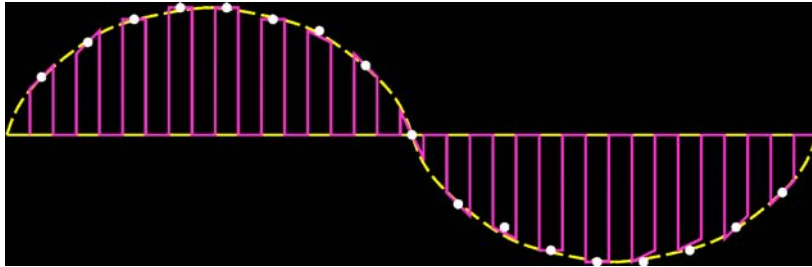
- **Convergence criterion**
 - Probe current equals zero
- **Advantages**
 - Autonomous circuit \Rightarrow forced circuit

$$Z(\omega) = \begin{cases} 0, & \omega = \omega_f \\ \infty, & \omega \neq \omega_f \end{cases}$$

E.Ngoya, *Int.J. Microw. Milim.-wave CAE*,1995

Mixed Time-Frequency Methods

- For circuits with both mild and strongly nonlinear behavior
 - Examples: switching mixer, switched-capacitor circuits

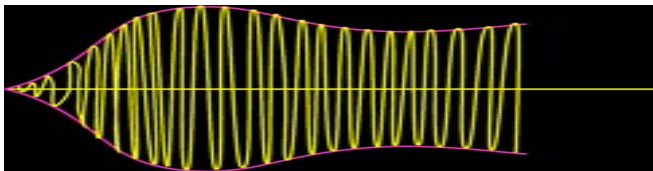


Mixed Time-Frequency Methods

- Represent the envelope waveform with few Fourier series terms
 - Few points needed to represent envelope
 - Can find them with a few transient simulations of the fast cycle
- New methods
 - Based on multi-rate partial differential equations
 - Uses bi-variate representations for efficient computation

Envelope Method

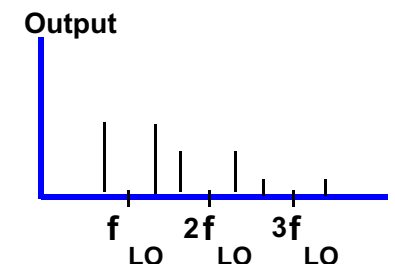
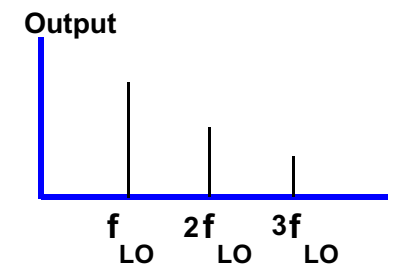
- Slow information signal over fast carrier
- Startup transients of circuits with fast signals
- AGC circuits, PLLs



- Direct calculation of envelope without tracing the fast cycles
 - Solve differential equation in the envelope
 - Inner loop is harmonic balance

Linear Time Varying Analysis

- Mixer example
 - RF=0 → [Mixer] ← LO
 - Periodic time varying network
- small signal → [Mixer] ← LO
 - Linear time varying network



Analysis Methods - Summary

	Time-Domain Methods	Frequency-Domain Methods	Mixed Time Freq. Method	Envelope Method	Linear Time Varying Method
Amplifiers (MNL)	X	X			
Amplifiers (HNL)	X				
Mixers (CT)	X	X	X		X*
Mixers (NCT)		X	X		X*
Oscillators	X	X		X	
PLLs, AGCs				X	
SC Circuits	X		X		X*

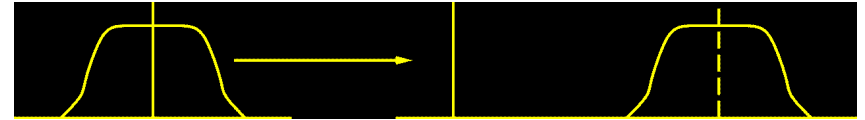
* Small signal

MNL = mildly nonlinear CT = commensurate tones

HNL = highly nonlinear NCT = noncommensurate tones

Mixing Noise

- Up/down conversion of noise due to mixing



- SPICE noise analysis does not work
- Cyclostationarity/frequency correlation important
- Monte Carlo or stochastic methods

Phase Noise

- Important for adjacent channel interference, data recovery, and sampled data systems
- Most analyses are of specific oscillators under simplifying assumptions
- Methods for proper phase noise calculation available in commercial simulators

Commercial RFIC Circuit Simulators

- Commercial simulators for RFIC design gaining maturity
- Simulators developed from two different fronts
 - Microwave design
 - ADS from Agilent/EEsof
 - Harmonica from Ansoft
 - Analog IC design
 - Spectre-RF from Cadence
 - ELDO-RF from Mentor

Conclusions

- **SPICE-like analyses not suitable for RFIC circuit simulation**
- **Fast and efficient RFIC simulation available in commercial simulators**
- **Available tools lack system on chip solutions**
- **Simulators need to be benchmarked for accuracy and performance**

Summary

- **Harmonic balance for**
 - High dynamic range weakly-nonlinear systems
 - RF front-ends (LNA, Mixer)
 - IQ modulators
 - LC and crystal oscillators
 - Circuits with distributed components
 - Transmission lines, S-parameter models
- **Time-domain PSS for**
 - Strongly nonlinear circuits
 - Ring oscillators
 - Frequency dividers
 - DC-DC converters
 - Input signals with sharp transitions